

# Techniques of Increasing Micro Grid Reliability

M. F. A. Omar, Dr. M. A. A. MEHANNA, Dr. Salah.K. EL-Sayed

Department of Electrical Engineering, Faculty of Engineering, Al-Azhar University, Cairo, Egypt.  
MFOMAR80@gmail.com

**Abstract**— One of the methods used today to increase power grids reliability is dividing the main (unified) grid to Micro Grid. This paper offers a study what is the technique that can be used to increase micro grid reliability. The reliability indices will be either customer base indices or energy sales base indices. The techniques will vary according to variable factors. Factors based on micro grid size, and the others based on the number of persons use this grid. The improvement impact for the different techniques will make the main map, which technique will be better for each micro grid. Techniques target the outage time & techniques target the outage loads.

**Index Terms**— Micro grid, System average interruption duration index, Customer average interruption duration index, Energy not supplied, Average energy not supplied, Renewable energy source, Photo voltaic, Mean time to transference switch, Mean time to repair.

## 1 INTRODUCTION

Now a day's utilities make an evolutionary change in the electricity infrastructure, and micro grids (MG) may hold that key to modernization and the realization of the Smart Grid. So the main factors affect the decision of this revolution in changing the mind from unified & centralized grid to micro grid is, how much there will be reliability improvement. What is the Micro Grid (M.G) & what is its size? A small scale system and located near the consumer is called the Micro-Grid (MG) system. The interconnection of small generation to low voltage distribution systems can be termed as the Micro Grid. Micro Grids can be operated with and without a connection to the main power network. [2]

Micro grid scale is variable scale according to zone where it could be self-dependent in the generated power [2,4]. In other word if it is disconnected (operate in the islanded mode) it will be self-dependent grid [2]. Micro grid scale could be limited also by the scale of distribution generation (DG) in range of (50K.V. A to 20 M.V.A). Reliability indices which will be focused in this paper could be divided into two categories. Customer Based Indices, and energy based indices [1]. Both of the two categories could be used to assess the past performance of the grid. As mentioned before the scale of the micro grid in this paper is limited within the common range of the available DG capacities in Egypt. There will be different modules of (MG) each module is identified according to the availability of operation in islanded mode forming micro grid. Techniques used also target the reliability indices improvement, which done by two ways minimize the outage time or minimize the outage loads.

## 2. RELIABILITY INDICES DEFINITION AND FORMULA

Customer Based Indices which are:

**SAIDI:** System Average Interruption Duration Index, indicates the total duration of interruption an average customer is subjected for a predefined time interval.

**CAIDI** Customer Average Interruption Duration Index, indicates the average time required to restore the service.

The other two indices are energy sales base indices which are:

**ENS** Energy not supplied by the system

**AENS** Average energy not supplied, AENS or Average system curtailment index, **ASCI** [1,4].

The reliability indices which will be measured by each technique will be calculated using the following input:

$\lambda_s = \sum_i \lambda_i$  (*failure rate*) it is the number of failure of the net work item per year..... (1)

$U_s = \sum_i \lambda_i \times r_i$  (Average Annual Outage Time) where  $r_i$  is the estimated time to repair. (2)

$r_s =$  (Average Outage Time/Repair time)..(3)

$N_i$  number of customers,  $L_i$  load value in KW ... (4)

According to those previous data the indices will be calculated as follow:

**SAIDI**= Sum of customers interruption duration / total no.of customers)  $\frac{\sum(U_i \times N_i)}{\sum(N_i)}$ (Hours/customer year)

**CAIDI**=Sum of customer interruption durations/total no. of customer interrupted  $\frac{\sum(U_i \times N_i)}{\sum(N_i \times \lambda_i)}$  (hours/customer interruption)

**ENS**=L(LOAD(KW))\*U (Outage duration) (KWh/yr)

$$= \sum(U_i \times L_i)$$

**AENS** (Average energy not supplied) calculated by dividing the ENS over the total number of customers  
 $= \sum(U_i \times L_i) / \sum(N_i)$  (KWH/CUSTOMERS/YR)

There are four techniques in this paper to improve reliability indices in micro grid. Those techniques are (Design technique, Operation technique) [1,5].

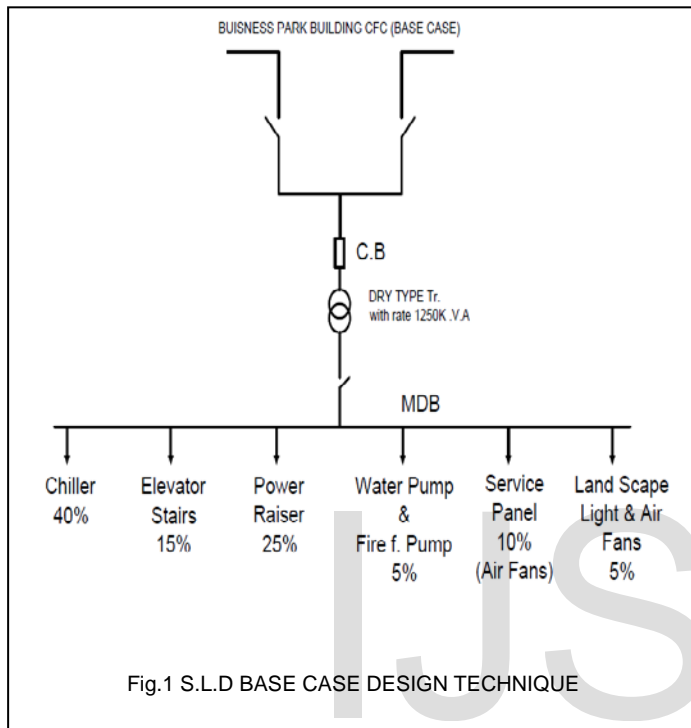


Fig.1 S.L.D BASE CASE DESIGN TECHNIQUE

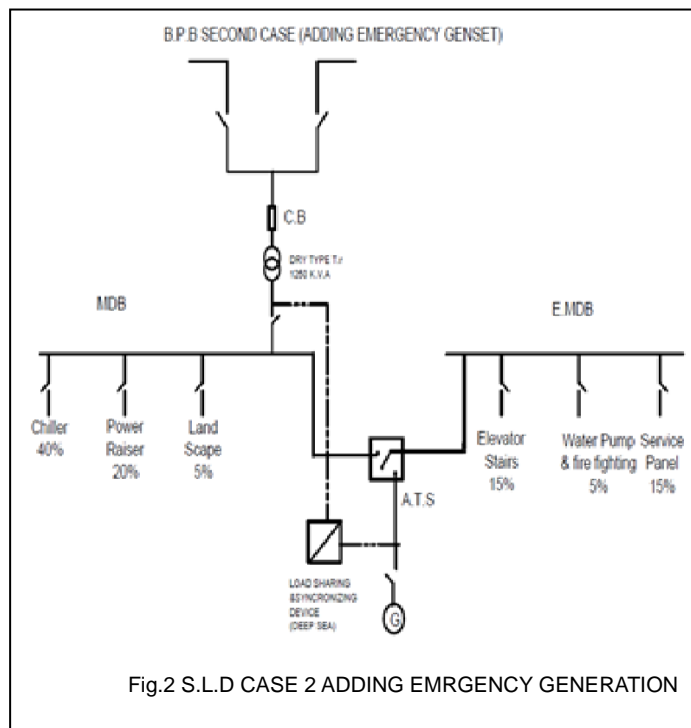


Fig.2 S.L.D CASE 2 ADDING EMRGENCY GENERATION

### 1-DESIGN TECHNIQUE (MINIMIZE OUTAGE LOAD)

This technique will be applied over two modules of micro grid scale. This technique studies the impact of using emergency generation, and RES Renewable Energy Source (PHOTO VOLTAIC ARRAY) on reliability indices.

#### 1.1 Module 1 commercial load small scale MG 650 K.V. A, 400 person

##### 1.1.1 Base Case

##### Module description

It is commercial load in new Cairo Egypt as shown in fig.1 where the building occupied by number of people nearly 400 persons the total load of the building is within 650K.V.A.

| ITEM TYPE      | Fail-ure/year( $\lambda$ ) | MTTR(hr.) | MTTS(h r.) |
|----------------|----------------------------|-----------|------------|
| R.M.U L.B.S    | 0.05                       | 1         | 0.116      |
| M.V.C.B        | 0.03                       | 3         |            |
| Tr.            | 0.015                      | 12        |            |
| L.V.M.C.B      | 0.03                       | 1         |            |
| Bus way raiser | 0.01                       | 2         |            |
| Main L.V cable | 0.02                       | 3         |            |

Table 1 – Component failure rate

According to data in table 1 and equations 1,2&3 indices could be calculated using the following data.

Data used in component failure rate based on two sources. Operation record where component number of failure over one year with respect to the predicted number of failure mentioned in the manufacturer specification. The manufacturer specification which usually relate the failure by (operating hours or number of switching)

Table2-Base Case Design technique indices calculation

| ITEM       | F/y $\lambda_i$ | MTTR $r_i$ | Us     | Li(kw) | Ni  | Ni * $\lambda_i$ | Us*Ni  | Li *Ui  |
|------------|-----------------|------------|--------|--------|-----|------------------|--------|---------|
| L.B.S      | 0.05            | 0.166      | 0.0083 | 750    | 400 | 20               | 3.32   | 6.225   |
| M.V.C.B    | 0.03            | 3          | 0.09   | 750    | 400 | 12               | 36     | 67.5    |
| Tr.        | 0.015           | 12         | 0.18   | 750    | 400 | 6                | 72     | 135     |
| L.V.C.B    | 0.03            | 1          | 0.03   | 750    | 400 | 12               | 12     | 22.5    |
| BUS RAISER | 0.01            | 2          | 0.02   | 750    | 400 | 4                | 8      | 15      |
| L.V CABLE  | 0.02            | 3          | 0.06   | 750    | 400 | 8                | 24     | 45      |
|            |                 |            |        |        |     | 62               | 155.32 | 291.225 |
| SAIDI      |                 | 0.39       |        |        |     |                  |        |         |
| CAIDI      |                 | 2.51       |        |        |     |                  |        |         |
| ENS        |                 | 291.23     |        |        |     |                  |        |         |
| AENS       |                 | 0.73       |        |        |     |                  |        |         |

**1.1.2 Second Case Adding Emergency Generator of 40% Loading.**

The only addition over table 1 the following data  
Generator failure rate:0.05  
MTTR (mean time to repair 1.2 hour)

Table 3 Case 2 Design Technique indices calculation

| ITEM       | F/y $\lambda_i$ | MTTR $r_i$ | Us     | Li(kw) | Ni  | Ni * $\lambda_i$ | Us*Ni  | Li *Ui   |
|------------|-----------------|------------|--------|--------|-----|------------------|--------|----------|
| L.B.S      | 0.05            | 0.166      | 0.0083 | 432    | 400 | 20               | 3.32   | 3.5856   |
| M.V.C.B    | 0.03            | 1.8        | 0.054  | 432    | 400 | 12               | 21.6   | 23.328   |
| Tr.        | 0.015           | 7.2        | 0.108  | 432    | 400 | 6                | 43.2   | 46.656   |
| L.V.C.B    | 0.03            | 0.6        | 0.018  | 750    | 400 | 12               | 7.2    | 13.5     |
| BUS RAISER | 0.01            | 2          | 0.02   | 750    | 400 | 4                | 8      | 15       |
| L.V CABLE  | 0.02            | 3          | 0.06   | 750    | 400 | 8                | 24     | 45       |
| D.G        | 0.05            | 1.2        | 0.06   | 288    | 400 | 20               | 24     | 17.28    |
|            |                 |            |        |        |     | 82               | 131.32 | 164.3496 |
| SAIDI      |                 | 0.33       |        |        |     |                  |        |          |
| CAIDI      |                 | 1.60       |        |        |     |                  |        |          |
| ENS        |                 | 164.35     |        |        |     |                  |        |          |
| AENS       |                 | 0.41       |        |        |     |                  |        |          |

**1.1.3 Case 3- Design technique adding RES unit with emergency generation.**

Adding RES (renewable energy source) with load share of 20% of total load. Since it is day light source there will be average value of share as it is non battery PV (photo voltaic) units it could be considered as 10% total load sharing.

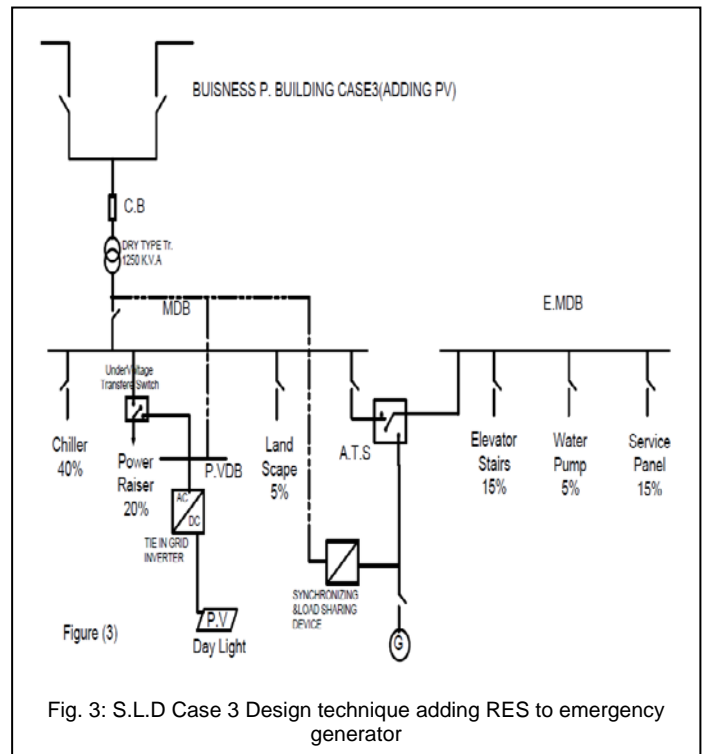


Figure (3) S.L.D Case 3 Design technique adding RES to emergency generator

|            | F/y $\lambda_i$ | MTTR $r_i$ | Us     | Li(kw) | Ni  | Ni * $\lambda_i$ | Us*Ni  | Li *Ui   |
|------------|-----------------|------------|--------|--------|-----|------------------|--------|----------|
| L.B.S      | 0.05            | 0.166      | 0.0083 | 375    | 400 | 20               | 3.32   | 3.1125   |
| M.V.C.B    | 0.03            | 1.8        | 0.054  | 375    | 400 | 12               | 21.6   | 20.25    |
| Tr.        | 0.015           | 7.2        | 0.108  | 375    | 400 | 6                | 43.2   | 40.5     |
| L.V.C.B    | 0.03            | 0.6        | 0.018  | 750    | 400 | 12               | 7.2    | 13.5     |
| BUS RAISER | 0.01            | 2          | 0.02   | 750    | 400 | 4                | 8      | 15       |
| L.V CABLE  | 0.02            | 3          | 0.06   | 750    | 400 | 8                | 24     | 45       |
| D.G        | 0.05            | 1.2        | 0.06   | 288    | 400 | 20               | 24     | 17.28    |
| PV SYSTEM  | 0.01            | 1          | 0.01   | 75     | 400 | 4                | 4      | 0.75     |
|            |                 |            |        |        |     | 86               | 135.32 | 155.3925 |
| SAIDI      |                 | 0.34       |        |        |     |                  |        |          |
| CAIDI      |                 | 1.57       |        |        |     |                  |        |          |
| ENS        |                 | 155.39     |        |        |     |                  |        |          |
| AENS       |                 | 0.39       |        |        |     |                  |        |          |

Table 5 comparison between 3 cases of Design technique indices calculation.

| Reliability indices comparison for previous three cases |                               |                               |                        |
|---|-------------------------------|-------------------------------|------------------------|
| Indices   | case 1 (without Genset & RES) | Case 2 E.Genset & without RES | Case 3 with Genset&RES |
| SAIDI   | 0.39                          | 0.33                          | 0.34                   |

| CAIDI | 2.51   | 1.60   | 1.57   | Tr. ROOM | Tr. Capacity (K.V.A) | LOADING FACTOR | LOAD AFTER DIVERSITY(K.V.A) | GEN.capacity (K.V.A) | GENSET %OF LOAD COVERAGE | % OF UN COVERED LOADS |
|-------|--------|--------|--------|----------|----------------------|----------------|-----------------------------|----------------------|--------------------------|-----------------------|
| ENS   | 291.23 | 164.35 | 155.39 | Tr. 1    | 1500                 | 70%            | 1050                        | 600                  | 57.14%                   | 42.86%                |
| AENS  | 0.73   | 0.41   | 0.39   | Tr. 2    | 2000                 | 65%            | 1300                        | 800                  | 61.54%                   | 38.46%                |
|       |        |        |        | Tr. 3    | 1000                 | 70%            | 700                         | 400                  | 57.14%                   | 42.86%                |
|       |        |        |        | Tr. 4    | 1500                 | 50%            | 750                         | 600                  | 80.00%                   | 20.00%                |
|       |        |        |        | Tr. 5    | 1500                 | 65%            | 975                         | 600                  | 61.54%                   | 38.46%                |
|       |        |        |        | Tr. 6    | 1500                 | 65%            | 975                         | 600                  | 61.54%                   | 38.46%                |
|       |        |        |        | sum      |                      |                | 5750                        |                      |                          |                       |

Table 6 Improvement percentage in case 2&case 3 Design technique

| Reliability indices | improvement after add GEN.40% load share | improvement after add RES 10% load share |
|---------------------|--|--|
| SAIDI               | 15.4%                                    | -3.0%                                    |
| CAIDI               | 36.3%                                    | 1.9%                                     |
| ENS                 | 43.6%                                    | 5.5%                                     |
| AENS                | 43.8%                                    | 5.1%                                     |

**1.2.1Module 2- case 1 (base case without add RES)**

Fig. 4 S.L.D show the residential load (Tr. Room configuration) with 40% load share of total load.

S.L.D of group of loads over M.V level as shown in figure 5

**1.2Module 2 Design Technique Residential Load With Total Load 5.750 M.V. A & 940 Person.**

In this module the indices calculation will be based on the following assumption:

The period of MTTs (mean time to transfer switching) between grid isolation and Gen. Startup is nearly 5min. 0.083 hr.

The MTTR (mean time to repair) if it is permanent fault in the main grid will be 2 hr.

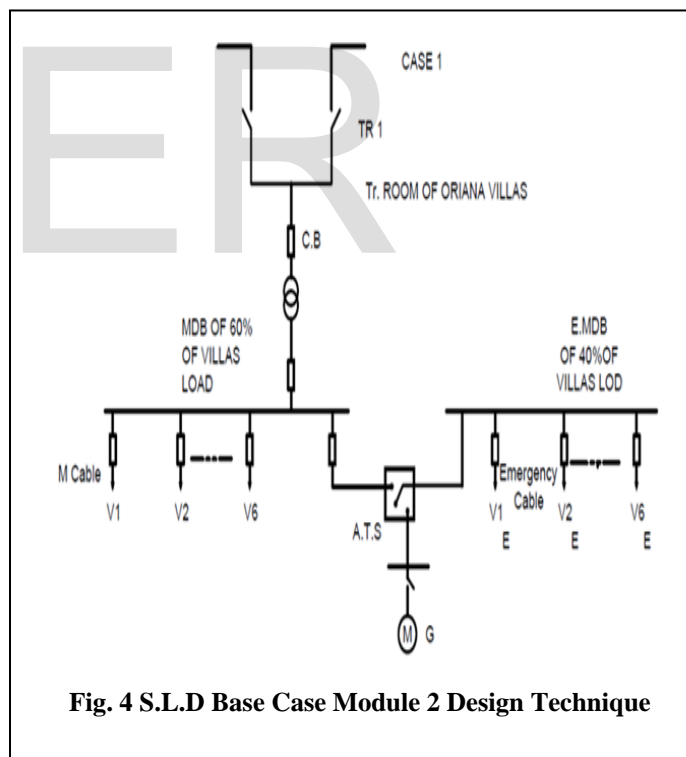
The repair time (rs) could be calculated using this formula.

$$(rs) = (0.083 \text{ hr.} * \text{GEN\%OF LOAD COVERAGE}) + (2\text{hr.} * \text{\%of un covered loads}) \dots (5)$$

Assume that Gen. (f/yr=5%) and percentage of Generator reliability95%.

$$Us (\text{outage time}) = [rs * 95\%] + [MTTR * 5\%]$$

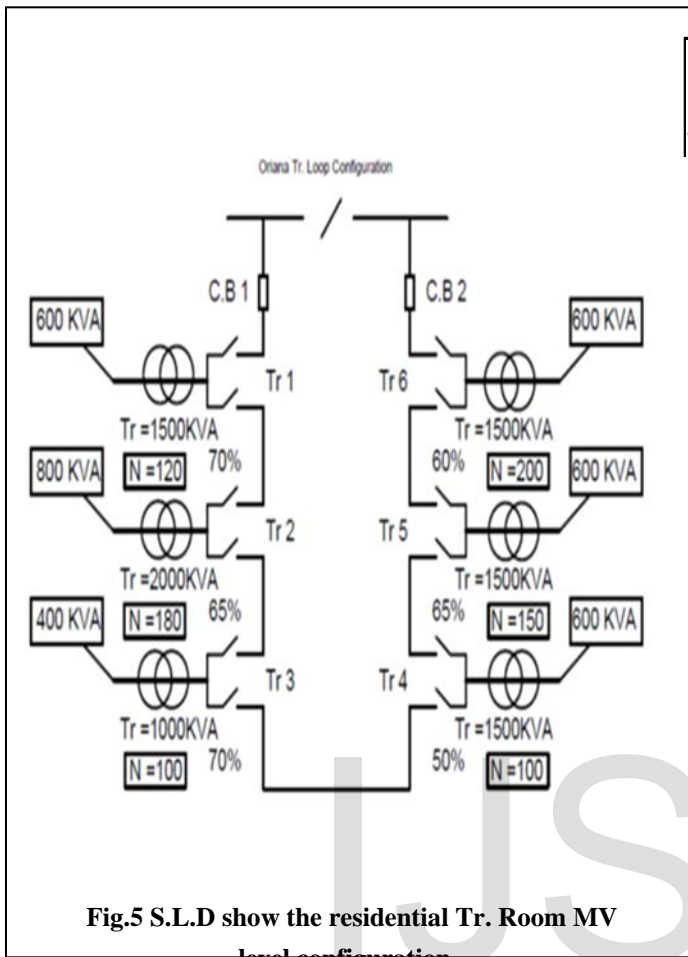
N is the no. of customers.



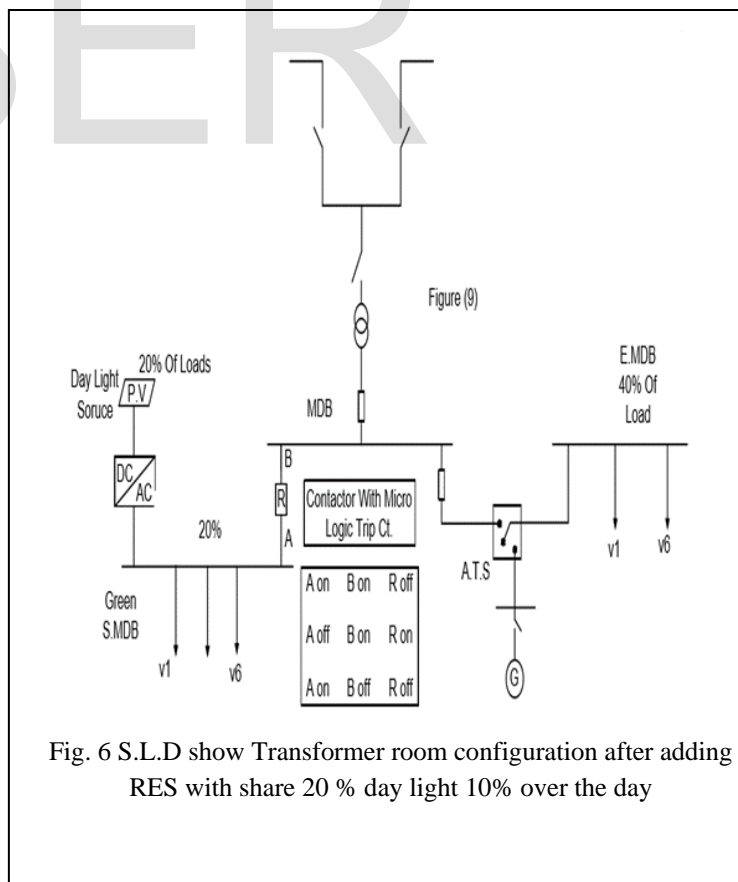
**Fig. 4 S.L.D Base Case Module 2 Design Technique**

Table7- Transformer Load & Percentage of Generator Coverage Module 2 Design Technique

Table 8-Module 2 Design Technique base case indices calculation



| Tr.ROOM | GENSET %OF LOAD COVERAGE | repair time FS | OUTAGE TIMEUs | LOAD AFTER DIVERSITY(K.W) | Ni  | Ni * $\lambda$ i | Us*Ni    | Li *Ui   |
|---------|--------------------------|----------------|---------------|---------------------------|-----|------------------|----------|----------|
| Tr.1    | 57.14%                   | 0.90457143     | 0.959343      | 1312.5                    | 120 | 6                | 115.1211 | 1259.138 |
| Tr.2    | 61.54%                   | 0.82030769     | 0.879292      | 1625                      | 180 | 9                | 158.2726 | 1428.85  |
| Tr.3    | 57.14%                   | 0.90457143     | 0.959343      | 875                       | 100 | 5                | 95.93429 | 839.425  |
| Tr.4    | 80.00%                   | 0.4664         | 0.54308       | 937.5                     | 100 | 5                | 54.308   | 509.1375 |
| Tr.5    | 61.54%                   | 0.82030769     | 0.879292      | 1218.75                   | 120 | 6                | 105.5151 | 1071.638 |
| Tr.6    | 61.54%                   | 0.82030769     | 0.879292      | 1218.75                   | 200 | 10               | 175.8585 | 1071.638 |
| SUM     |                          |                |               | 7187.5                    | 940 | 41               | 705.0096 | 6179.825 |
|         |                          |                |               |                           |     |                  |          |          |
|         |                          |                |               |                           |     |                  |          |          |
|         | SAIDI                    | 0.75           |               |                           |     |                  |          |          |
|         | CAIDI                    | 17.20          |               |                           |     |                  |          |          |
|         | ENS                      | 6179.83        |               |                           |     |                  |          |          |
|         | AENS                     | 6.57           |               |                           |     |                  |          |          |



**. Case 2 Module 2 Design Technique Adding RES with Load Sharing 10 % of Total Load.**

As shown in Fig. 6 after add RES to transformer room to share the loads by 10% as shown in fig.6.

**Table 9 Case 2 Module2 Reliability Indices Calculation**

| Tr.ROOM | GENSET %OF LOAD COVERAGE | % OF UN COVERED LOADS | repair time fS | OUTAGE TIMEUs | LOAD AFTER DIVERSITY(K.W) | Ni  | Ni *Xi | Us*Ni    | Li *Ui   |
|---------|--------------------------|-----------------------|----------------|---------------|---------------------------|-----|--------|----------|----------|
| Tr.1    | 71.43%                   | 32.86%                | 0.716429       | 0.780607      | 1312.5                    | 120 | 6      | 93.67286 | 1024.547 |
| Tr.2    | 76.92%                   | 28.46%                | 0.633077       | 0.701423      | 1625                      | 180 | 9      | 126.2562 | 1139.813 |
| Tr.3    | 71.43%                   | 32.86%                | 0.716429       | 0.780607      | 875                       | 100 | 5      | 78.06071 | 683.0313 |
| Tr.4    | 100.00%                  | 10.00%                | 0.283          | 0.36885       | 937.5                     | 100 | 5      | 36.885   | 345.7969 |
| Tr.5    | 76.92%                   | 28.46%                | 0.633077       | 0.701423      | 1218.75                   | 120 | 6      | 84.17077 | 854.8594 |
| Tr.6    | 76.92%                   | 28.46%                | 0.633077       | 0.701423      | 1218.75                   | 200 | 10     | 140.2846 | 854.8594 |
| SUM     |                          |                       |                |               |                           | 940 | 41     | 559.3301 | 4902.906 |
|         | SAIDI                    |                       | 0.60           |               |                           |     |        |          |          |
|         | CAIDI                    |                       | 13.64          |               |                           |     |        |          |          |
|         | ENS                      |                       | 4902.91        |               |                           |     |        |          |          |
|         | AENS                     |                       | 5.22           |               |                           |     |        |          |          |

**Table10 Reliability indices improvement before and after adding RES.**

| comparing reliability indices for the two experiment modules |                             |                          |                       |
|--|-----------------------------|--------------------------|-----------------------|
| Reliability Indices  | Oriana module 1 without RES | Oriana module 2 with RES | Improvem ent percent. |
| SAIDI  | 0.75                        | 0.60                     | 20.67%                |
| CAIDI  | 17.20                       | 13.64                    | 20.70%                |
| ENS  | 6466.25                     | 4902.91                  | 24.18%                |
| AENS   | 6.57                        | 5.22                     | 24.18%                |

**Second Technique (Operation Technique) (Minimize Outage Time)**

**Module Description**

In this case there will be a sample on the M.V level of CFC grid, and in case of emergency where the two shown loop are isolated from the rest of loops forming Micro Grid. Here are some facts about this micro grid:  
1-It is shown that there are three types of load in this micro grid:

First: Residential loads, second: Business building, third: facilities load.

2-There will be total number of customers will be 8700 customers.

3-This micro grid will be only provided with protection devices C.B at the start and the end of the loops. This module will face two faults in the same time as follow:

First the M.V cable of the loop had permanent fault of insulation failure

Second the Circuit Breaker (C.B) of loop2 is out of duty due to chamber insulation failure.

This scenario from the registration data is considered one of the worst scenario the customer face in outage time.

**Case 1-base case (M.G without Tie in cable) 8700 persons 6.208 M.V. A**

| Tr.ROOM        | GENSET %OF LOAD COVERAGE | % OF UN COVERED LOADS | repair time fS | OUTAGE TIMEUs | LOAD AFTER DIVERSITY(K.V.A) | LOAD AFTER DIVERSITY(K.W) | Ni   | Ni *Xi | Us*Ni    | Li *Ui   |
|----------------|--------------------------|-----------------------|----------------|---------------|-----------------------------|---------------------------|------|--------|----------|----------|
| B.P1           | 57.14%                   | 42.86%                | 0.261714       | 0.34862857    | 1050                        | 1312.5                    | 600  | 30     | 209.1771 | 457.575  |
| B.P2           | 80.00%                   | 20.00%                | 0.1664         | 0.25808       | 750                         | 937.5                     | 400  | 20     | 103.232  | 241.95   |
| B.P3           | 66.67%                   | 33.33%                | 0.222          | 0.3109        | 900                         | 1125                      | 500  | 25     | 155.45   | 349.7625 |
| B.P4           | 50.00%                   | 50.00%                | 0.2915         | 0.376925      | 1200                        | 1500                      | 800  | 40     | 301.54   | 565.3875 |
| HONDA          | 61.54%                   | 38.46%                | 0.243385       | 0.33121538    | 650                         | 812.5                     | 200  | 10     | 66.24308 | 269.1125 |
| TOYOTA         | 61.54%                   | 38.46%                | 0.243385       | 0.33121538    | 650                         | 812.5                     | 200  | 10     | 66.24308 | 269.1125 |
| WATER STATION  | 0.5                      | 0.5                   | 0.2915         | 0.376925      | 504                         | 630                       | 3000 | 150    | 1130.775 | 237.4628 |
| SEWAGE STATION | 0.5                      | 0.5                   | 0.2915         | 0.376925      | 504                         | 630                       | 3000 | 150    | 1130.775 | 237.4628 |
| sum            |                          |                       |                |               | 6208                        | 7760                      | 8700 | 435    | 3163.435 | 2627.826 |
|                | SAIDI                    |                       | 0.363613       |               |                             |                           |      |        |          |          |
|                | CAIDI                    |                       | 7.272265       |               |                             |                           |      |        |          |          |
|                | ENS                      |                       | 2627.826       |               |                             |                           |      |        |          |          |
|                | AENS                     |                       | 0.302049       |               |                             |                           |      |        |          |          |

Table 11 Case 1 Operation Technique Reliability indices calculation

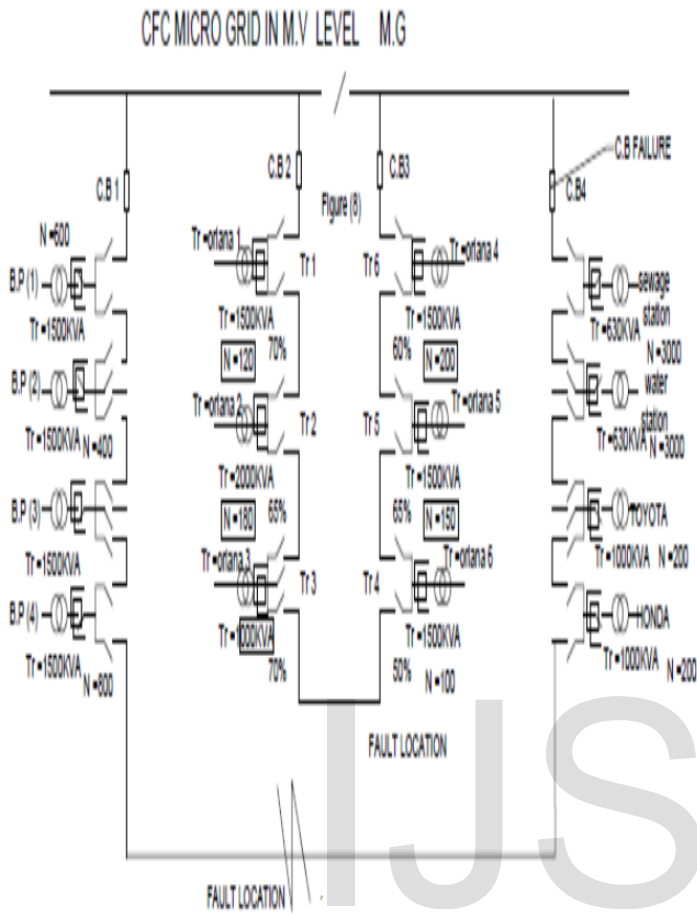


Fig.7 S.L.D of Case 1 Operation Technique Without Add Tie in Cable

General Facts about the case study  
 In this case the MTTR=2 hour (for loads from sewage to Honda) because of the following:  
 The feeding system is radial feeding as C.B.4 at the other side of the loop is failed due to insulation break down.

The time needed to identify the fault location will be 30 min regardless it's physical location (this is due to the manual strategy for fault location identification).

We chose the path of the tie in cable to be satisfy the following (the shortest distance for the economic impact, the mid load point for the two loops as possible)

It is the most effective case where the tie in cable minimize the outage time clearly.

Tie in cable could represent emergency cable for loads.

There must be adjustment for protection devices after adding the tie in cable taking in consideration the injection current value.

This technique could also be called (current injection technique) where current injected from loop to other increasing the reliability indices of both loops.

This technique could be used over the M.V&L.V level (MG).

**Case 2-base case (M.G Adding Tie in cable)**

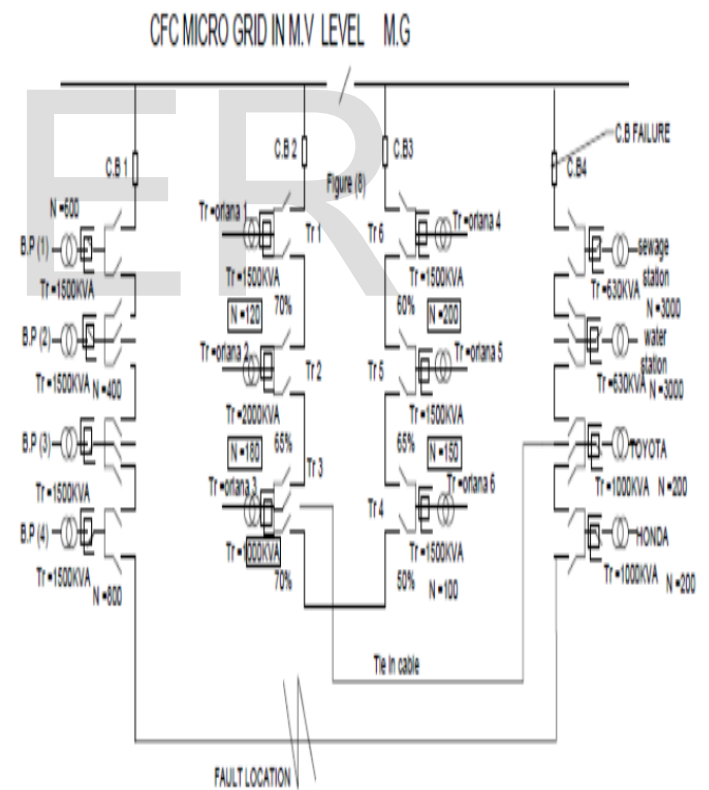


Fig.8 S.L.D of Case 2 Operation Technique Add Tie in Cable

| Tr.ROOM           | GENSET<br>%OF LOAD<br>COVERAGE | % OF UN<br>COVERED<br>LOADS | repair<br>time FS | OUTAGE<br>TIMEUs | LOAD AFTER<br>DIVERSITY(K.<br>V.A) | LOAD AFTER<br>DIVERSITY(K.<br>W) | Ni<br>Ni *%i | Us*Ni | Li *Ui   |          |
|-------------------|--------------------------------|-----------------------------|-------------------|------------------|------------------------------------|----------------------------------|--------------|-------|----------|----------|
| B.P1              | 57.14%                         | 42.86%                      | 0.154571          | 0.15934286       | 1050                               | 1312.5                           | 600          | 30    | 95.60571 | 209.1375 |
| B.P2              | 80.00%                         | 20.00%                      | 0.1164            | 0.12308          | 750                                | 937.5                            | 400          | 20    | 49.232   | 115.3875 |
| B.P3              | 66.67%                         | 33.33%                      | 0.138667          | 0.14423333       | 900                                | 1125                             | 500          | 25    | 72.11667 | 162.2625 |
| B.P4              | 50.00%                         | 50.00%                      | 0.1665            | 0.170675         | 1200                               | 1500                             | 800          | 40    | 136.54   | 256.0125 |
| HONDA             | 61.54%                         | 38.46%                      | 0.147231          | 0.15236923       | 650                                | 812.5                            | 200          | 10    | 30.47385 | 123.8    |
| TOYOTA            | 61.54%                         | 38.46%                      | 0.147231          | 0.15236923       | 650                                | 812.5                            | 200          | 10    | 30.47385 | 123.8    |
| WATER<br>STATION  | 0.5                            | 0.5                         | 0.1665            | 0.170675         | 504                                | 630                              | 3000         | 150   | 512.025  | 107.5253 |
| SEWAGE<br>STATION | 0.5                            | 0.5                         | 0.1665            | 0.170675         | 504                                | 630                              | 3000         | 150   | 512.025  | 107.5253 |
|                   |                                |                             |                   |                  |                                    |                                  | 8700         | 435   | 1438.492 | 1205.451 |
|                   | SAIDI                          |                             | 0.165344          |                  |                                    |                                  |              |       |          |          |
|                   | CAIDI                          |                             | 3.306878          |                  |                                    |                                  |              |       |          |          |
|                   | ENS                            |                             | 1205.451          |                  |                                    |                                  |              |       |          |          |
|                   | AENS                           |                             | 0.138558          |                  |                                    |                                  |              |       |          |          |

Table 12 Case 2 Operation Technique Reliability indices calculation

| Reliability indices                           | SAIDI<br>hr./<br>customer yr | SAIDI<br>hr./custome<br>r yr | SAIDI<br>hr./custo<br>mer yr | SAIDI<br>hr./custome<br>r yr |
|---|------------------------------|------------------------------|------------------------------|------------------------------|
| M.G without tie in cable between<br>M.V loops | 0.90                         | 17.60                        | 4416.20                      | 0.51                         |
| M.G with tie in cable between<br>M.V loops    | 0.30                         | 5.02                         | 1503.50                      | 0.17                         |
| improvement percentage                        | 66.67%                       | 71.48%                       | 65.95%                       | 66.67%                       |

Table 13 Reliability indices improvement with and without tie in cable

## CONCLUSION

### Design Technique (load sharing technique) minimize the load outage

This achieved by adding emergency generation with ratio near to 40% of total loads, and adding RES (renewable energy source) PV (photo voltaic arrays) with load share average 10 % of total loads. And we conclude that adding RES had LOW IMPACT on reliability indices for small scale micro grid (less than 2M.V. A). The failure rate of the micro grid component also could be taken in consideration in indices calculation for small scale micro grid, but in large scale micro grid the component failure rate could be neglected.

### (operation technique) or (current injection technique) minimize outage time

This achieved by installing tie in cable. This technique found other feeding source to the disconnected loads.

The following conclusion about the micro grid could be taken in consideration as follow:

- 1- Micro grid is limited grid could be self-dependent at any time when disconnected from the main grid this is called (islanded mode).
- 2- It is not condition to be in islanded mode, but we could make the improvement in connected mode (connected to the main grid).
- 3- It is preferred than the unified system because it is more controllable than the unified grid.



- 4- It has variable scale not limited with certain size  
the only limitation that it could be self-dependent  
in case of islanding mode.
- 5- The researcher estimate that the average scale  
depend on common distribution generation scale  
is 20 M.V.A.
- 6- Any improvement in reliability will directly af-  
fect the customer as it is more adjacent and direct  
affect the customer need.

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